

STRESS MAGNIFICATIONS IN WALLS WITH OPENINGS

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This paper is a part of a larger effort (1) to establish the relationships between the parameters of a wall opening (such as aspect ratio, position, and area), and the rigidity and strength of one-storey walls with single openings under earthquake loads. The walls are analyzed as plane stress problems assuming linearly elastic isotropic material and small deformations. For the analysis ELAS75 (2) computer program is used. In this paper, walls having the aspect ratio of 1/2 with openings of aspect ratios 1/1 and 1/2 are studied with different sizes and positions, under uniformly distributed unit horizontal static loading. Stress magnification factors for 16 cases (out of 148 in the original work) are presented, and the effects of opening size increments on the maximum stress magnification factors are graphically shown.

In seismic regions, in addition to the gravity loads, buildings are subjected to earthquake accelerations causing large inertial forces, many times during their lifetime. The resultant of the gravity loads and the instantaneous seismic loads caused by the earthquake accelerations may be considered as an inclined gravitational force. The degree of its inclination from the vertical is a function of the horizontal component of the seismic acceleration. It is the horizontal component of the seismic accelerations which is of great concern in the design of load bearing walls. In this work only this horizontal component is considered.

The following assumptions are made:

1. The wall is a single storey load bearing outer wall which has a single opening.
2. The opening is rectangular in shape.
3. The cross walls are on the same side and at the ends only.
4. The wall is clamped at the bottom, and carries a reinforced concrete slab at the top.
5. The wall material is linearly elastic homogeneous and isotropic.
6. The wall is subjected to a uniformly distributed unit horizontal static load in its plane at its upper edge.

The wall is shown in Fig. 1. Along the top and vertical edges thicknesses are varied to represent the stiffness of the cross walls and the slab. The responses of the idealized walls under unit loads are obtained by plane stress analysis, using the ELAS75 program. The program computes the responses by the displacement method of analysis and the finite element method. The key sketch of the wall with the finite element mesh producing less than 2% discretization error in the stresses is shown in Fig. 2. The program computes the displacements and the stresses at the mesh points. The standard

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program is modified for this work to produce not only stresses σ_{xx} , σ_{yy} , σ_{xy} but also the principal stresses σ_1 , σ_2 , and the angle that σ_2 (smaller principal stress) makes with the horizontal direction.

The values of the wall parameters for the 16 cases studied in this work are given in Table I. The computer printouts for the stress magnification factors of these cases are presented in Figs. 3-6. The stress magnification factor at a wall point is defined as the ratio of the maximum shear stress at that point of the wall with opening to that of the corresponding wall without opening. Considering the largest magnification factor in the wall as the maximum magnification factor, the variation of this factor with the opening percentage (i.e., the ratio of the opening area to the wall area) is shown in Figs. 7-10.

From the results of this work, the following may be concluded:

- i . The maximum stress magnification factor increases with an increasing rate as the opening percentage increases.
- ii . The maximum stress magnification factor increases as the opening moves upward.
- iii. The maximum stress magnification factor increases as the aspect ratio of the opening changes from 1/1 to 2/1.

Acknowledgements

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References

- (1) Utku, B., Morphotectonic Relationships Between Walloping-Wall, Walloping-Reinforcement in Loadbearing Single Storey Brick Walls with Single Openings, in Earthquake Areas (Deprem Bölgelerindeki Tek Katlı, Tek Boşluklu Taşıyıcı Tuğla Duvarlarda Boşluk-Duvar, Boşluk-Donatı Morfotektonik İlişkileri), Doctoral Dissertation, İstanbul Technical University, 1977.
- (2) Utku, S., Instructor's Manual for Part II of Elementary Structural Analysis, Norris, Wilbur, Utku, 3rd Ed., McGraw-Hill Book Company, New York, 1976.

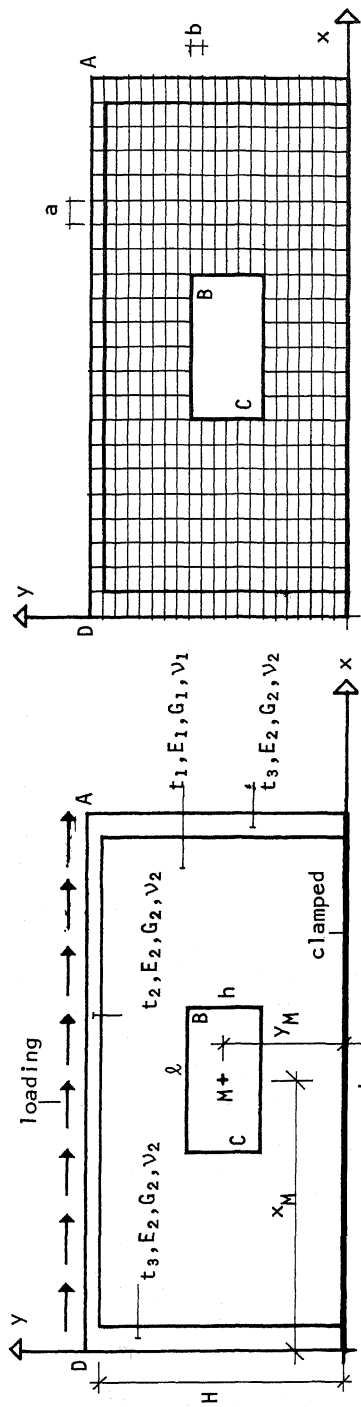


Figure 1. Idealized wall

Figure 2. Key sketch

Table 1. VALUES OF WALL PARAMETERS

wall label	W1	W2	W3	W4	W5	W6	W7	W8	W9	W10	W11	W12	W13	W14	W15	W16	
parameters	ranges of parameters																
opening (%)	4	9	16	36	2	8	18	32	2	8	18	32	2	8	18	32	
l/h	<	2	>	<	1												>
x_M	<	11 a			>	15 a			>	11 a			>	11 a			
y_M	<	10 b			>	20 b			>	4b			>	6b			
H	<	2			>	2			>	2			>	8b			
L/H	<	1			>	1			>	1			>	1			
t_1	<	5			>	5			>	5			>	5			
t_2/t_1	<	3			>	3			>	3			>	3			
t_3/t_1	<	1			>	1			>	1			>	1			
E_2/E_1	<	1			>	1			>	1			>	1			
G_2/G_1	<	1			>	1			>	1			>	1			
$\nu_1=\nu_2$	<	1/4			>	1/4			>	1/4			>	1/4			

t_1 : wall thickness ;
 t_2, t_3 : thicknesses in the boundary zones
 E_1, E_2 : wall and boundary Young's Moduli
 G_1, G_2 : wall and boundary Shear Moduli
 ν_1, ν_2 : wall and boundary Poisson's ratios
 a : horizontal meshsize (DDX in printouts)
 b : vertical meshsize (DDY in printouts)

RIG TABLE
 JPL-23, JPL-25, JPL-26, JPL-27, JPL-28, JPL-29, JPL-30, JPL-31, JPL-32, JPL-33, JPL-34, JPL-35, JPL-36, JPL-37, JPL-38, JPL-39, JPL-40
 ITC= 9 DMS= 0.10002 30 DVM= 5.50000-01
 ITC= 7 DMS= 0.10002 01 DVM= 5.50000-01
 ITC= 5 DMS= 0.10002 01 DVM= 5.50000-01
 ITC= 3 DMS= 0.10002 01 DVM= 5.50000-01
 ITC= 1 DMS= 0.10002 01 DVM= 5.50000-01
 ALL ERRORS ARE SCALED BY 10** 2

0	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
20	99	100	99	97	95	94	93	92	91	90	89	88	87	86	85	84	83	82	81	80	79
18	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86	85	84	83	82	81
16	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86	85	84	83
14	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86	85
12	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87
10	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89
8	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91
6	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93
4	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95
2	117	116	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97
0	119	118	117	116	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99

W5

RIG TABLE
 JPL-23, JPL-25, JPL-26, JPL-27, JPL-28, JPL-29, JPL-30, JPL-31, JPL-32, JPL-33, JPL-34, JPL-35, JPL-36, JPL-37, JPL-38, JPL-39, JPL-40
 ITC= 9 DMS= 0.10002 30 DVM= 5.50000-01
 ITC= 7 DMS= 0.10002 01 DVM= 5.50000-01
 ITC= 5 DMS= 0.10002 01 DVM= 5.50000-01
 ITC= 3 DMS= 0.10002 01 DVM= 5.50000-01
 ITC= 1 DMS= 0.10002 01 DVM= 5.50000-01
 ALL ERRORS ARE SCALED BY 10** 2

0	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
20	99	100	99	97	95	94	93	92	91	90	89	88	87	86	85	84	83	82	81	80	79
18	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86	85	84	83	82	81
16	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86	85	84	83
14	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86	85
12	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87
10	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89
8	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91
6	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93
4	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95
2	117	116	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97
0	119	118	117	116	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99

W7

RIG TABLE
 JPL-23, JPL-25, JPL-26, JPL-27, JPL-28, JPL-29, JPL-30, JPL-31, JPL-32, JPL-33, JPL-34, JPL-35, JPL-36, JPL-37, JPL-38, JPL-39, JPL-40
 ITC= 7 DMS= 0.10002 03 DVM= 5.50000-01
 ITC= 5 DMS= 0.10002 01 DVM= 5.50000-01
 ITC= 3 DMS= 0.10002 01 DVM= 5.50000-01
 ITC= 1 DMS= 0.10002 01 DVM= 5.50000-01
 ALL ERRORS ARE SCALED BY 10** 2

0	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
20	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86	85	84	83	82	81	80
18	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86	85	84	83	82
16	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86	85	84
14	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88	87	86
12	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90	89	88
10	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92	91	90
8	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94	93	92
6	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96	95	94
4	116	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98	97	96
2	118	117	116	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100	99	98
0	120	119	118	117	116	115	114	113	112	111	110	109	108	107	106	105	104	103	102	101	100

W6

RIG TABLE
 JPL-23, JPL-25, JPL-26, JPL-27, JPL-28, JPL-29, JPL-30, JPL-31, JPL-32, JPL-33, JPL-34, JPL-35, JPL-36, JPL-37, JPL-38, JPL-39, JPL-40
 ITC= 3 DMS= 0.10002 03 DVM= 5.50000-01
 ITC= 1 DMS= 0.10002 01 DVM= 5.50000-01
 ALL ERRORS ARE SCALED BY 10** 2

0	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
20	152	138	113	86	68	56	55	161	158	145	145	158	161	55	56	68	86	113	138	152	161
18	155	145	129	116	110	112	82	206	147	110	96	110	147	206	82	112	116	129	145	155	161
16	172	163	155	158	175	202	197	245	158	78	5	78	158	245	197	202	175	158	155	163	172
14	189	184	182	199	211	241	169														
12	210	201	202	209	213	177	128														
10	235	231	227	220	196	131	84														
8	245	246	231	219	187	125	91														
6	249	239	232	217	181	126	108														
4	248	245	231	214	181	133	130														
2	242	232	222	206	181	158	180														
0	239	224	218	201	184	174	207														
20	226	211	201	194	191	208	273														
18	219	202	191	187	193	236	310														
16	218	193	187	182	190	258	359														
14	205	183	167	162	180	258	408														
12	200	172	150	142	157	210	271	15	6	1	6	15	6	15	81	271	408	150	172	200	271
10	199	154	117	121	104	104	222	109	26	6	9	26	109	222	109	165	121	117	154	199	271
8	170	141	105	103	116	236	240	125	55	18	11	55	125	240	205	126	105	141	170	271	271

W8

Figure 4. Computer printouts for walls W5, W6, W7, W8

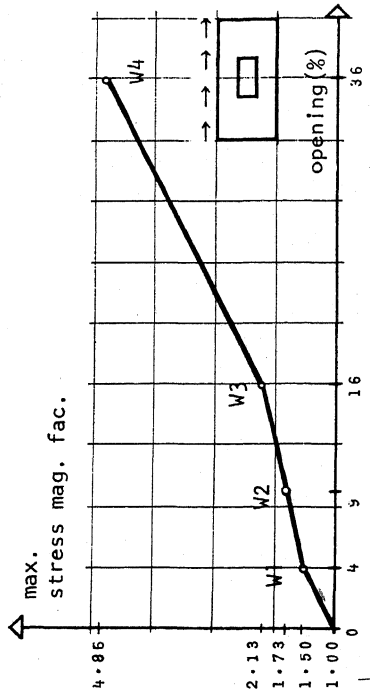


Figure 7. Opening percentage versus max.smf for walls W1, W2, W3, W4

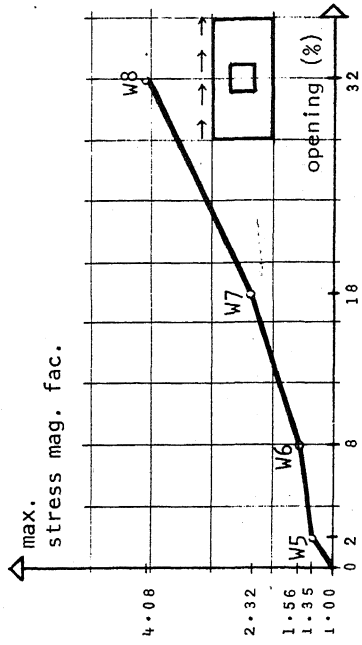


Figure 8. Opening percentage versus max.smf for walls W5, W6, W7, W8

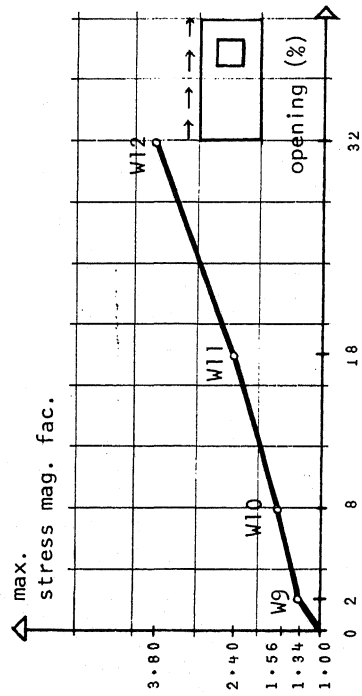


Figure 9. Opening percentage versus max.smf for walls W9, W10, W11, W12

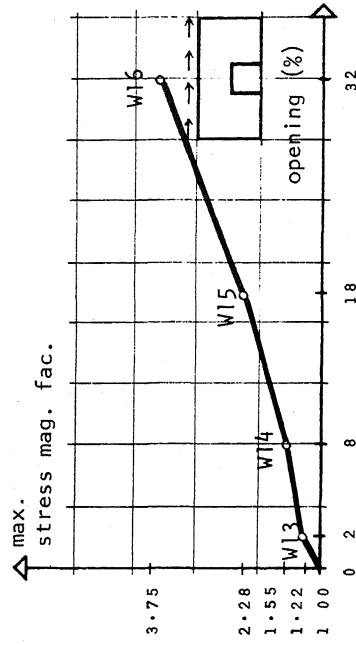


Figure 10. Opening percentage versus max.smf for walls W13, W14, W15, W16