

THEORETICAL AND OBSERVATIONAL INVESTIGATION OF STRUCTURAL  
RESPONSE TO INSTANTANEOUS PEAK ACCELERATIONS DURING STRONG EARTHQUAKES

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S Y N O P S I S

A sinusoidal earthquake motion is considered with a sudden acceleration increment at its n-th period and the response of a one degree of freedom structure is theoretically investigated by successive application of the final conditions of one stage as initial conditions of the following stage. The results are compared with recorded strong motion accelerograms of this type and the corresponding acceleration and displacement response spectra. Some conclusions are derived concerning the validity of the theoretical results as well as the structural behaviour for transient forced vibration of this type.

1. Theoretical formulation

An ideal sinusoidal earthquake motion as indicated in Fig.1 is considered. Stages 1, lasting n periods, and 3, have the same frequencies ( $\omega$ ) and amplitudes ( $\alpha_1$ ) while stage 2 occurring after stage 1 and consisting of only one period is showing the same frequency ( $\omega$ ) but an amplitude  $\alpha_2 = v\alpha_1$  ( $v > 1$ ).

The equation of the motion of a single degree of freedom undamped system subjected to the above mentioned sinusoidal motion for the stage i, is :

$$\ddot{x}_i + \omega_0^2 x_i = \alpha_i \sin \omega t_i \quad (1)$$

where  $\omega_0$  the natural frequency of the system.

The general solution of equation (1) is given by the formula :

$$x_i = \frac{A_i}{\cos \psi_i} \sin(\omega_0 t_i + \psi_i) + \frac{x_{st}}{1 - \frac{\omega^2}{\omega_0^2}} \sin \omega t_i \quad (2)$$

$$\dot{x}_i = \frac{A_i \omega_0}{\cos \psi_i} \cos(\omega_0 t_i + \psi_i) + \frac{x_{st} \omega}{1 - \frac{\omega^2}{\omega_0^2}} \cos \omega t_i \quad (3)$$

where  $x_{st} = \frac{\alpha_1}{\omega_0^2}$  is the displacement of the system under a static load  $\alpha_1$  m, and  $A_i, \psi_i$  constants depending on the initial conditions of each stage.

By the successive application of the final conditions of stage i as initial conditions to stage i+1, omitting in this description the intermediate operations, we obtain the following formulae for  $\max x_i$ , occurring at time intervals where  $\dot{x}_i = 0$ .

$$\frac{\max x_i}{x_{st}} = \frac{1}{1 - \frac{\omega^2}{\omega_0^2}} \left[ -\frac{\omega}{\omega_0} \sin \frac{2k\pi}{1 + \frac{\omega}{\omega_0}} + \sin \frac{\omega}{\omega_0} \frac{2k\pi}{1 + \frac{\omega}{\omega_0}} \right] \quad (4)$$

$$\frac{\max \chi_2}{\chi_{st}} = \frac{1}{1 - \frac{\omega^2}{\omega_0^2}} \left[ -\frac{\omega}{\omega_0} v \operatorname{tg} \lambda_2 \sin(k\pi - \frac{\pi}{2} - \lambda_2) + v \sin \frac{\omega}{\omega_0} (k\pi - \frac{\pi}{2} - \lambda_2 - \psi_2) \right] \quad (5)$$

$$\text{where } \operatorname{tg} \psi_2 = \frac{\sin \omega_0 nT}{v - 1 + \cos \omega_0 nT} \quad (6)$$

$$\text{and } \operatorname{tg} \lambda_2 = \frac{v - 1 + \cos \omega_0 nT}{v \cos \psi_2} \quad (7)$$

$$\frac{\max \chi_3}{\chi_{st}} = \frac{1}{1 - \frac{\omega^2}{\omega_0^2}} \left[ -\frac{\omega}{\omega_0} \operatorname{tg} \lambda_3 \cos(k\pi - \lambda_3) - \cos \frac{\omega}{\omega_0} (k\pi - \lambda_3 - \psi_3) \right] \quad (8)$$

$$\text{where : } \operatorname{tg} \psi_3 = \frac{v \operatorname{tg} \lambda_2 \sin(\omega_0 T + \psi_2)}{v \operatorname{tg} \lambda_2 \cos(\omega_0 T + \psi_2) + v + 1} \quad (9)$$

$$\text{and } \operatorname{tg} \lambda_3 = -\frac{1}{\cos \psi_3} \{v \operatorname{tg} \lambda_2 \cos(\omega_0 T + \psi_2) + v + 1\} \quad (10)$$

Applying to formulae (4), (5) and (8) for different values of  $\frac{\omega}{\omega_0}$ ,  $v$  and  $n$  the curves showed in Fig.2 are obtained, giving the corresponding values of  $\frac{\max \chi_i}{\chi_{st}}$

## 2. Comparison with real strong earthquakes

Two characteristic earthquakes of similar type with the above examined ideal sinusoidal earthquake motion are investigated.

### a) Parkfield (U.S.A.) earthquake occurred in June 27, 1966

From the accelerogram showed in Fig.3 we obtain  $\alpha_1 = 0,108 \text{ g}$ ,  $\alpha_2 = 0,50 \text{ g}$ ,

$$v = \frac{0,50}{0,108} = 4,63, \quad T = 0,692, \quad n = 3.$$

From the corresponding acceleration and displacement response spectra (Fig. 4 and 5), we obtain for a structure with natural period  $T_0 = 1 \text{ sec}$ ,  $\omega_b = 6,28 \text{ sec}^{-1}$ ,  $\max \chi = 17 \text{ cm}$ .

For this structure  $\chi_{st} = 2,686 \text{ cm}$ . From the curves of Fig.2 and for  $\frac{\omega}{\omega_0} = \frac{T_0}{T} = \frac{1,00}{0,692} = 1,445$  we obtain  $\frac{\max \chi}{\chi_{st}} = 6,33$  and  $\max \chi = 6,33 \times 2,686 = 17 \text{ cm}$ .

### b) Leukas (Greece) earthquake occurred in November 4, 1973

Compared with Parkfield earthquake, having an almost constant amplitude at stages 1 and 3, Leukas earthquake is showing an irregularity of the variation of its amplitude (Fig.6). In order to obtain a sinusoidal form convenient for the application of the above theoretical formulae, the use of a Fourier analysis gave four harmonics with periods in sec., 0,415, 0,83, 1,25, 1,66, which coincides with the values resulting from the displacement and acceleration response spectra (Fig. 7, 8)

For a structure with natural period  $T_0 = 1 \text{ sec}$ ,  $\max \chi$  results according to the following table :

T	$\omega$	$\frac{\omega}{\omega_0}$	$\nu$	n	$\alpha_1$	$X_{st}$	$\frac{\max X}{X_{st}}$	max X
0,415	15,73	2,59	6,8	9	0,078g	0,31	3	0,93
0,830	7,56	1,30	2,1	4,5	0,053g	0,84	12	10,08
1,25	5,04	0,86	1,0	2,25	0,031g	1,11	6	6,66
1,66	3,79	0,65	1,0	1,125	0,0124g	0,787	2,25	1,77

max  $\chi$  = 19,44

The displacement response spectrum gives a value of max  $\chi$  = 20 cm.

### 3. Conclusions

a) The above theoretical formulae are giving satisfactory results in cases of accelerograms of the type of figure 1, with almost constant amplitude in stages 1 and 3.

b) In cases of varying amplitudes a Fourier spectral analysis is recommended and the total max. displacement is the sum of max  $\chi$  of each harmonic component.

c) The influence of the instantaneous acceleration peak to the structure, is limited during only the time interval of the acceleration increment, without having any effect on stage 3.

d) The sequence of occurrence of peak acceleration does not affect considerably the overcharge of the structure, except of a range near resonance, where this influence is considerable.

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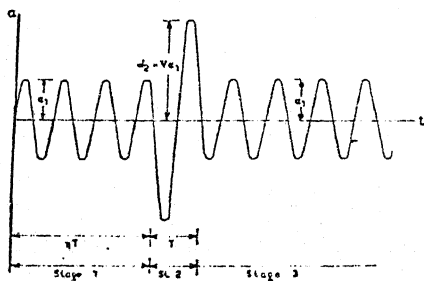


Fig. 1

