Development of an Electronic Fuel Injection System for a 4-stroke Locomotive Diesel Engine of Indian Railways

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Introduction
There are about 1000 WDM2 locomotives (Rated power: 2600 hp) working for the Indian Railways, which is a upgraded ALCO locomotive engine. The ALCO locomotive engines are rebuilt after 18 years of active service, and they are then upgraded to a higher power rating of 3100 hp. Technical specifications of the locomotive engine after power uprating are given in Table 1.

Table 1: Technical specifications of upgraded locomotive engine

<table>
<thead>
<tr>
<th>Configuration</th>
<th>V-16, DI, 4S, Turbocharged, Inter-cooled Diesel engine</th>
</tr>
</thead>
<tbody>
<tr>
<td>Bore/Stroke</td>
<td>228.6/ 266.7 (mm)</td>
</tr>
<tr>
<td>Displacement</td>
<td>10.95 liter/ cylinder</td>
</tr>
<tr>
<td>Compression Ratio</td>
<td>11.75 (static)</td>
</tr>
<tr>
<td>Fuel Injection Equipment</td>
<td>Mechanical pump line nozzle (PLN) system</td>
</tr>
<tr>
<td>Nozzle Opening Pressure</td>
<td>250 bar</td>
</tr>
<tr>
<td>Rated Power</td>
<td>2312 kW @ 1050 rpm</td>
</tr>
<tr>
<td>Torque at max. speed</td>
<td>22000 Nm @ 1050 rpm</td>
</tr>
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</table>

These ALCO design locomotive engines are fitted with a higher capacity mechanical fuel injection system during these upgrades. ALCO engines use a Pump-Line-Nozzle (PLN) system for fuel injection into the cylinder. The original fuel injection pumps used on
ALCO Engines has a plunger diameter of 15 mm. The plunger diameter of the fuel injection pump was increased from 15 mm to 17 mm by RDSO in order to have higher fuel injection flow rate at higher fuel injection pressures. This modification resulted in increase of peak fuel line pressure from 750 to 1000 bars which improved the fuel efficiency. The existing mechanical fuel injection system of the engine consists of three main components, namely fuel injection pump; high pressure tubing which connects the fuel injection pump to the nozzle and; fuel injection nozzle. The fuel injection pump is mounted on the fuel pump support, which is mounted on the side of the engine crankcase. The pump is actuated by the fuel cam lobe of the camshaft through a lever arm and roller. The pump has a ported barrel and constant-stroke plunger incorporating bottom helix for fuel delivery control. The pump primarily consists of a housing, delivery valve and spring, delivery valve holder, element (plunger and barrel assembly), plunger spring, a geared control sleeve and control rack (rod) assembly. The pump element comprise of a barrel and plunger, which are matched, and assembled with a very close tolerance. The fuel injection pump has three functions: (a) to raise the fuel supply pressure to a value, which will efficiently atomize the fuel, (b) to supply the correct quantity of fuel to the injection nozzle commensurate with the power and speed requirements of the engine, and (c) to accurately time the delivery of the fuel for efficient and economical operation of the engine. The nozzle is a low sac design with nine fuel injection holes. The fuel is injected into a quiescent combustion chamber; therefore the penetration of the injected spray is largely dependent on the injection characteristics of the injector nozzle and the pump injection pressure.

Mechanical fuel injection system however is not capable to precisely time the delivery of the fuel based on the engine load and speed requirement. With only a fuel delivery helix in the fuel injection pump plunger, the fuel injection timing cannot be varied. As engine speed and load decreases, the injection timing should be retarded to have optimum location of cylinder pressure peak. The mechanical fuel injection system can be optimized only for the rated speed and load because of its limitations therefore at all other engine operating points, the fuel injection is done in a sub-optimum manner.

In a mechanical fuel injection system, response time during transient engine operation is longer, which results in over-fueling/ under-fueling and black sooty smoke emission is observed during engine transients, which is a visual and environmental nuisance. For load control, the mechanical system has to depend on the engine governor, control-shaft and linkages, which are prone to defects and require regular adjustments. The reliability of the mechanical fuel injection system
is also therefore adversely affected due to large number of such moving parts. By machining an additional helix on the top of the plunger (top helix), some fixed control of the injection timing was achieved. However with an electronic fuel injection system, there is complete flexibility in varying the start of fuel delivery to obtain an optimum pressure curve and low smoke opacity theoretically and electronic fuel injection systems also offer enormous flexibility to the process of fuel injection. In view of all these advantages offered by electronic fuel injection system, it was decided to experiment retrofitting ALCO WDM2 locomotives with Electronically Controlled Fuel Injection system (EFI) during the mid-life rebuilding.

**Background**

In view of the advantages offered by an electronic fuel injection system in comparison to mechanical fuel injection system, a collaborative research project by the Engine Development Directorate, Research Designs and Standards Organization under the Ministry of Railways and Engine Research Laboratory (ERL), Indian Institute of Technology Kanpur was conceptualized. IIT Kanpur was contacted by EDD, RDSO to help them develop Electronic Fuel injection System for the ALCO DLW Locomotive series, which is the main workhorse of the Indian Railways. The collaboration started in year 2010 with major focus on developing an interface of the EFI system with the engine test cells at RDSO for optimization of the engine and calibration of the ECU and for interfacing and integration of the EFI system to the locomotive traction control system and assist RDSO in overall integration of the EFI system on to a diesel locomotive. Engine Research Laboratory of IIT Kanpur undertook this work and delivered the EFI for the Locomotive successfully in association with EDD, RDSO in less than 4 months.

**Project Objectives**

Following project objectives were identified for this collaborative project to be executed by ERL, IIT Kanpur:

- Design and development of a suitable hardware and software for interfacing of EFI system to the AVL make control test stand in the Engine Development Directorate at RDSO.
- Assist RDSO in the optimization of the engine and ECU calibration in solving problems associated with integrated load and speed control of the engine.
Design and develop suitable hardware and software for integrating the EFI system to a locomotive traction control system for fitment on a diesel locomotive.

Provide support to RDSO and DMW Patiala teams during the integration of EFI onto the prototype diesel locomotive.

Trouble-shoot any problems reported during the field trials of the locomotive.

Implementation

Design and development of hardware and software for the project were carried out by ERL, IIT Kanpur with close involvement of Engine Development Directorate, RDSO, Lucknow.

As a first step, a detailed study of the AVL test bed control system was done. A conflict in the communication protocols between the AVL system and Heinzmann ECU was discovered. This was set right by developing a suitable design of hardware and software. An interface box was manufactured by ERL with these specifications. The AVL test controller did not specify the ports to be used for external communication, therefore special efforts were made to configure a port to be able to communicate to the Heinzmann ECU. After installing the interfacing box, problems were rectified and an integrated control of engine speed and load was established on the Test-bed. Engine was operated and optimized at each engine load and speed point and the ECU calibrated accordingly. After successful calibration of the ECU on the engine test bed, attention was focused towards designing and developing an interfacing hardware and software for installation of the EFI on a diesel locomotive. This was done by ERL in a record time and the Engine Development Directorate team successfully completed the trials on running a diesel locomotive at Alambagh diesel shed, Lucknow. Three shift working for close to two weeks were required to initially establish the efficacy of the interfacing box design on the locomotive. Based on the inputs received during ‘dry run’ of the EFI on a locomotive at Alambagh diesel shed, further design modifications were carried out on the system and a new interfacing box was manufactured for fitment on the prototype diesel locomotive at DMW Patiala. At DMW, ERL team supervised the fitment of the interfacing box on the locomotive and provided valuable assistance to the RDSO and DMW team in integrating the complete system on the locomotive and finally made a working proto-type. First prototype diesel locomotive was finally flagged off from DMW in the month September 2010.
System Overview

Figure 1: Block Diagram of the EFI system integrated to Locomotive Control System

Error! Reference source not found. Figure 1 shows the block diagram of the electronically controlled fuel injection system as fitted on the locomotive. Parameters such as engine speed, cam position, engine boost air pressure, lubricating oil pressure and coolant temperature are acquired by the engine control unit (ECU). Engine fueling is controlled by the ECU by systematically energizing the magnetic valves fitted on the fuel injection pumps. Drive to the fuel injection pump is through the camshaft and a lever mechanism Error! Reference source not found. A schematic of the PLN system is shown in figure 2.

Figure 2: Pump Pipe Nozzle System of Indian Railway’s ALCO DLW Locomotives

The diesel engine on the locomotive is mechanically coupled to an alternator. Electrical power generated by the alternator is used by the traction motors fitted on the locomotive axles to provide traction power to the diesel locomotive. The load on the engine is controlled by varying the field current of the alternator; engine fuelling and speed is controlled by the ECU. In response to the driver’s notch handle and/or road conditions, the loading and fuelling of the engine are varied to maintain a pre-determined engine
speed at each engine notch. There are nine engine notches, starting from Idle to the 8th engine notch having specific engine speed and power output. The power, torque generated by the engine vis-à-vis engine speed for the locomotive is shown in Figure 3.

![Engine Speed vs. Torque and Power](image)

**Figure 3: Engine torque, power and speed at different engine notches**

Using EFI, it is possible to adjust the fuel injection timing according to varying load and speed conditions of the engine dynamically so as to achieve extremely low fuel consumption and efficient engine operation with lowest pollution. These tasks cannot be performed by a mechanical fuel injection system. The advantages of EFI system over mechanical fuel injection system include:

(a) digital setting of parameters, (b) precise and dynamic control of injection timings, injection duration, (c) elimination of mechanical hardware, (d) protection of engine, (e) online fault diagnostics, display and logging of faults, (f) optimized fuel injection for each cylinder and every engine operating point depending on load and speed condition, (g) reduction in smoke opacity levels and particulate matter, (h) possibility of cut-off of fuel to individual cylinders, and (i) protection against hot engine, automatic cut-off of load and fuel and enhanced safety and flexibility.
Schematic of the EFI system is shown in Figure 4. EFI System for ALCO engine consists of Electronic Fuel Injection Pump(s), Engine Control Unit (ECU), Sensors (Lube oil, Speed, Boost Pressure, Water Temperature), Wiring harness, Injectors, High pressure pipe and fuel galleries, filters, Check valve/ Pressure control valves etc. Before fitment on the locomotive, it is imperative to map the diesel engine with the EFI on a research test bed. The research engine test bed at RDSO Engine Development Directorate (EDD) had a microprocessor based test bed controller. The ECU of the fuel system must communicate with the Test controller for testing on the test bed. During the course of testing, it was noticed that the ECU of the EFI cannot be interfaced with the test controller due to difference in hardware and software and will require developing a separate hardware and software for the same. However, it was possible to run the engine by separately controlling the EFI and the test bed controller. Load control was implemented by the test bed controller and the engine speed control separately by the ECU of the EFI system. However for transient operation optimization, it was required to have unified load and speed control from the test bed controller. For this, it was essential to have an interface between the test bed controller and the ECU of EFI. At the same time, it was required to finally fit the EFI onto a diesel locomotive for carrying out the field trials. For this also, it was needed to interface the EFI ECU to the microprocessor based locomotive traction system computer.

On the Test-bed, in the present mechanical fuel injection system, two fuel control shafts were actuated by the Engine Actuator using servo motors. These control shafts control the rotational movement of the mechanical fuel injection pump plungers. This rotated the helix on the FIP plunger and changes the effective stroke and delivered fuel quantity. The operating system of the Test-bed controls the engine by load control by
hydraulic dynamometer control and engine speed by fuel control through the fuel actuator. The system has a number of channels for analog and digital inputs and outputs.

The requirement was to interface the ECU to the operating system of the test cell controller such that test cell controller can control the ECU. Since the ECU is controlling the speed of the engine, the way to send the speed set value from the test cell controller to the ECU had to be found.

**Locomotive ECU Calibration**

Control circuit structure for the EFI is shown in Figure 5.

![Control Circuit structure for the EFI system](Error! Reference source not found.)

A speed set-point is received by the speed governor (ECU) and based on the PID map and injection quantity map, an injection quantity is calculated. This injection quantity is then limited by additional maps such as boost air pressure, engine water temperature, lube oil pressure and temperature etc. Based on the limited injection quantity calculation, an injection duration and start of injection are calculated from predetermined maps. The engine speed and cam phasing are measured by employing suitable sensors and are used in the feedback loop. These form the basis for feedback loop control of the engine speed vis-à-vis the engine speed set-point and the firing order of the engine. The magnetic valves on the fuel injection pumps are energized based on the firing order map of the engine. For ECU calibration it is required to create different fuel limitation and safety maps for the engine.
At different fuel injection quantities, the engine rpm was varied and the fuel injection duration in CAD was recorded on the ECU’s DC Desk software. A map was thus created, which was saved into the calibration maps of the ECU (Figure 6). This exercise was repeated at different SOP timings and the injection duration at each combination of fuel quantity and engine speed was plotted respectively. The ECU calculates the injection duration at a particular speed and load by interpolating the values from these four maps. This injection duration is used to determine the solenoid energizing duration.

Figure 6: Delivery period map notch-wise, SOP at 33.5° BTDC

Brake specific fuel consumption (bsfc) vis-a-vis fuel delivery start timing sweeps were carried out to obtain the most suitable start of fuel delivery at different engine notches. This is shown in figure 7. Brake specific fuel consumption was found to be lowest at different SOP timing for different engine notches. SOP timing with the lowest bsfc was used to program the ECU of the EFI.

Figure 7: Bsfc at different fuel delivery start angles for different engine notches
Start of pumping map is shown in Figure 8. In this Map, x-axis shows the engine speed, y-axis shows the delivered fuel quantity in mm$^3$/stroke. The z-axis gives the start of pumping or beginning of delivery. Notable is that as the engine speed decreases, the start of pumping gets retarded in order to operate at the optimum point of operation.

![Figure 8: Delivery begin MAP (SOP) in the EFI software](image)

**Engine performance**

Figures 9-10 present the reduction in bsfc and the smoke opacity levels on engine fitted with EFI in comparison to the mechanical FI.

![Figure 9: Comparison of brake specific fuel consumption of EFI and Mechanical System](image)
Figure 10: Comparison of smoke opacity levels of EFI and Mechanical Systems

EFI system delivers 4.1% fuel saving in passenger duty cycle and 3.97% in freight duty cycle. Apart from the fuel saving, there is 70% reduction in smoke opacity of the locomotive exhaust. The black smoke emissions from the locomotive were completely eliminated, even during transient operating conditions.

Reasons for the improvement in the brake specific fuel consumption and the reduction in the smoke opacity levels were further investigated by studying the fuel line pressure, needle lift, in-cylinder pressure and the heat release rates in comparison to the mechanical fuel injection system. These are shown in tables 2-3.

Table 2: Comparison of the fuel line pressure, injector needle lift and the in-cylinder pressures with EFI and mechanical FI fitted engines
Table 2 shows that the EFI has been able to retard the fuel injection timing at lower engine notches. This resulted in optimum development of in-cylinder pressures at all engine notches. At higher engine notches, the fuel injection timing with EFI had to be advanced because of smaller plunger diameter of the EFI as compared to mechanical FI. Instantaneous heat release rates in the cylinder also indicate that the fitment and calibration of EFI has been able to shift the heat release rates to optimum points for maximum utilization of the fuel energy. Retarding the fuel injection timing with EFI pump lead to longer fuel injection pulse width and increase in total hydrocarbons (THCs) in exhaust and increase in exhaust temperatures (beyond design limit) due to after-burning of hydrocarbons. Thus a case exists to increase the plunger diameter of the EFI pump. This will help in increasing the mean effective injection pressure (MEIP) of the EFI pump and expected to reduce the emissions of THCs and reduce the bsfc ever further.

Table 3: Comparison of the instantaneous heat release between EFI and mechanical FI fitted engines
After detailed calibration of the EFI on the research test bed, the system was fitted on the locomotive. For this, the ECU of the EFI was interfaced with the Traction control system of the locomotive. Locomotive was successfully run with this arrangement and put into service with reduction in fuel consumption (over control locomotive) by about 4% and emission reduction of more than 70% in field service.

**Concluding Remarks**

An Electronic fuel injection system has been developed for the diesel locomotive. This involved design and development of suitable interfaces between the ECU of the EFI and the Test cell controller and the Locomotive traction control computer, mapping of the engine and determination of optimum fuel injection quantities and start of fuel delivery. A reduction in fuel consumption of 4% has been achieved by fitment of EFI to the locomotive, also a significant reduction of smoke opacity levels has been achieved. The main outcome of this collaborative project resulted in the following:
1. Development of Electronic Fuel Injection for the ALCO Locomotive, to replace the widely used mechanical injection system, which makes precise injection of fuel possible to match the demand of load, optimize fuel consumption and cuts down emissions.

2. *Saving of 4% of High Speed Diesel* over the duty cycle of the diesel locomotive. This is over and above that achieved due to upgrades already made on the locomotives. *The potential saving is enormous, considering the Indian Railways consume nearly 250 Crore litres of fuel costing approximately Rs 13,000 Crores.*

3. Complete elimination of black smoke from locomotive engine. This not only saves the environment, but also saves fuel, since black smoke is caused by incompletely burnt fuel.

4. Elimination of hot engine failures of the locomotives.

5. Elimination of large number of mechanical components, reduction in maintenance and increase in reliability.


This fete is achieved purely indigenously due to collaborative efforts of *RDSO and IIT Kanpur*. This landmark project heralds “greening” of diesel traction in the true sense. It also marks the culmination of the synergic teamwork of industry and academia previously unseen on Indian Railways and opens the doors to numerous such possible collaborations in the future.

**References**


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Contacts

Prof. Avinash Kumar Agarwal joined Department of Mechanical Engineering, Indian Institute of Technology Kanpur in 2001. His areas of interest are IC engines, combustion, alternative fuels, biodiesel, alcohol, natural gas, hydrogen, conventional fuels, lubricating oil tribology, emission control, optical diagnostic techniques, laser ignition, HCCI, particulates, micro-sensors, and large bore engines. Prof. Agarwal has recently been designated as Fellow of SAE International, USA in class of 2013. He is recipient of several prestigious national and international awards such as “NASI-Reliance Industries Platinum Jubilee Award-2012” for Application Oriented Innovations in Physical Sciences; INAE Silver Jubilee Young Engineer Award-2012; Dr. C. V. Raman Young Teachers Award: 2011 for Excellence in the field of Engineering Education; SAE International’s Ralph R. Teetor Educational Award -2008; INSA Young Scientist Award-2007; UICT Young Scientist Award-2007 by University Institute of Chemical Technology, Mumbai; INAE Young Engineer Award-2005; AICTE Career Award for Young Teachers-2004; DST Young Scientist Award-2002; and DST BOYSCAST Fellowship. IIT Kanpur recognized him as “Poonam and Prabhu Goyal Chair Professor (2013-16)” for his contributions in the field of Energy.

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Dr. Anirudh Gautam is Executive Director (Engine Development) at RDSO, Lucknow. He is working for Indian Railways Service (Mechanical Engineers) since 1986. Dr. Gautam joined Indian Railways as a special class railway apprentice (SCRA 1983 batch) at Jamalpur. Dr. Gautam received his M.E. in Engine Systems from University of Wisconsin, Madison, USA in 2010 and he obtained his PhD in IC Engines from IIT Kanpur in 2013. He developed the first hotel load diesel locomotive for export and carried out the indigenisation of the EMD locomotive technology at DLW. Dr. Gautam was also responsible for upgradation of horsepower of EMD locomotives from 4000 hp to 4500 hp. Dr. Gautam has been actively involved in the IR projects on alternate fuels and emission reduction of diesel locomotives. He is currently working on development of dual fuel CNG diesel locomotive for IR.

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Photo Gallery

13th August 2011, DMW Patiala

13th August 2011, DMW Patiala
14th September, 2011, Alambagh Diesel Shed, Lucknow

14th September, 2011, DG, RDSO Flagging off at Alambagh Diesel Shed, Lucknow