

# Lecture 4: Experiment 3

## EE380 (Control Systems)

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# Announcements

- Before doing an experiment, download latest versions of supporting documents from Brihaspati.
- Turn off power supply to board when not programming dsPIC or taking readings.
- After completion of experiment
  - Shut down PC, FG, PS.
  - Remove PICkit 2 from dsPIC board.

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# Procedure of Exp.3



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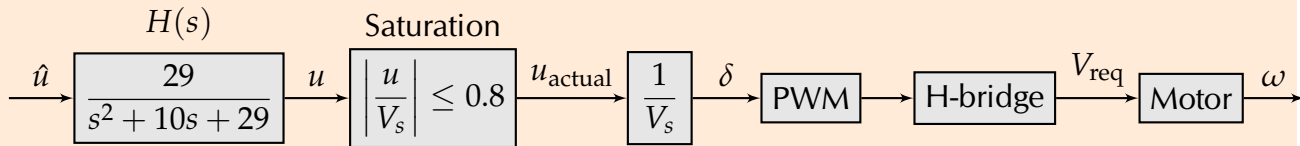
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# Outline of the experiment

Want speed of motor to track a reference step. Steps:

- Convert plant into 3rd order by prefixing 2nd order TF.



Here,  $\hat{u}$  is controller's output,  $u_{\text{actual}}$  is numerical value of voltage applied to motor's armature.  $V_{\text{req}}$  is actual voltage applied to motor's armature,  $\delta$  is duty ratio of PWM signal.

- Apply step & tune  $k_p$  so that CL system's output oscillates sustainably.
- Determine coefficients of P, PI, PID controllers.
- Observe CL system's response to step under P, PI, PID control.



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# Tasks common to all 6 experiments

## Simulation

- Perform PC-based simulation of CL system using GNU Octave.
- Perform PC-based simulation of digital control of a continuous-time system using GNU Octave.

## Realization on hardware

- Utilize the various components of an integrated development environment (IDE): editor, compiler, linker, debugger, and programmer to program a  $\mu$ C.
- Program controller using C language into  $\mu$ C.
- Monitoring: read data into PC from  $\mu$ C using UART modules.

## Analysis

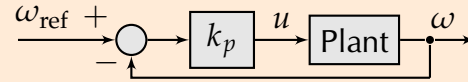
- Compare actual performance with predicted performance.

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## Second Ziegler-Nichols method

Applies to plants exhibiting sustained oscillations in CL proportional control for some  $k_p = k_{cr} > 0$ .

**Step 1:** Form CL system with  $k_p > 0$ .



**Step 2:** Apply step  $\omega_{\text{ref}}$  to CL system and record  $\omega$ .

**Step 3:** With  $\omega_{\text{ref}}$  on, increase  $k_p$  from 0 to  $k_{cr}$ .

**Step 4:** Determine period  $P_{cr}$  of oscillations.

**Step 5:** Tune parameters of PID controller according to table.

Type of controller	$k_p$	$T_i$	$T_D$
P	$0.5k_{cr}$	$\infty$	0
PI	$0.45k_{cr}$	$(1/1.2)P_{cr}$	0
PID	$0.6k_{cr}$	$0.5P_{cr}$	$0.125P_{cr}$



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# Homework (HW) vs. Lab work (LW)

HW

Prefix  $\frac{29}{s^2+10s+29}$   
to math model from Exp.1

Determine  $k_{cr}$  &  $P_{cr}$

Determine P, PI, PID controllers

Simulate using tf, step, easysim.m

Comment on observations

Descretize & code in C  
 $H(s)$  and controllers

LW

Program  $H(s)$  into dsPIC

Form CL sys with  $k_p$   
Apply step  $\omega_{ref}$   
Tune  $k_p$  until sustained oscillations  
Determine  $k_{cr}, P_{cr}$

Determine PID controller

Simulate using easysim.m

Program PID controller & verify

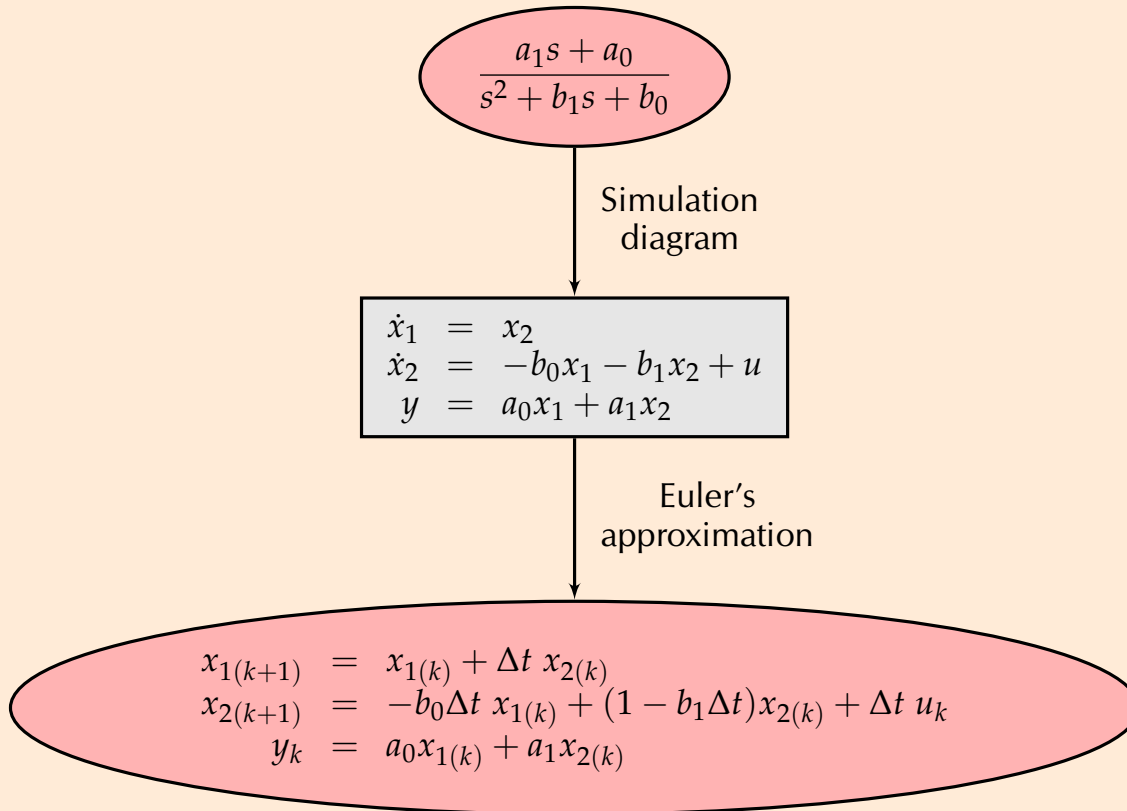


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# Discretization



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# Simulate; LW: C code, Implement, Analyze

- Simulation: `easysim.m`
- Discretized controller  
→ C code:
- Implement: As in demo slides
- Analyze: Compare results

$$\begin{aligned}x_1(k+1) &= a_{11}x_1(k) + a_{12}x_2(k) + b_1u(k) \\x_2(k+1) &= a_{21}x_1(k) + a_{22}x_2(k) + b_2u(k) \\y(k) &= c_1x_1(k) + c_2x_2(k) + du(k)\end{aligned}$$

In `main-prog.c` before `main()` insert `float x1[2],x2[2];`  
In `main()` insert `x1[0] = x2[0] = 0;`

```
x1[1] = a11 * x1[0] + a12 * x2[0] + b1 * u;
x2[1] = a21 * x1[0] + a22 * x2[0] + b2 * u;
y = c1 * x1[0] + c2 * x2[0] + d * u;
x1[0] = x1[1];
x2[0] = x2[1];
```



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# Review of Exp.2: Least squares sys-id theory

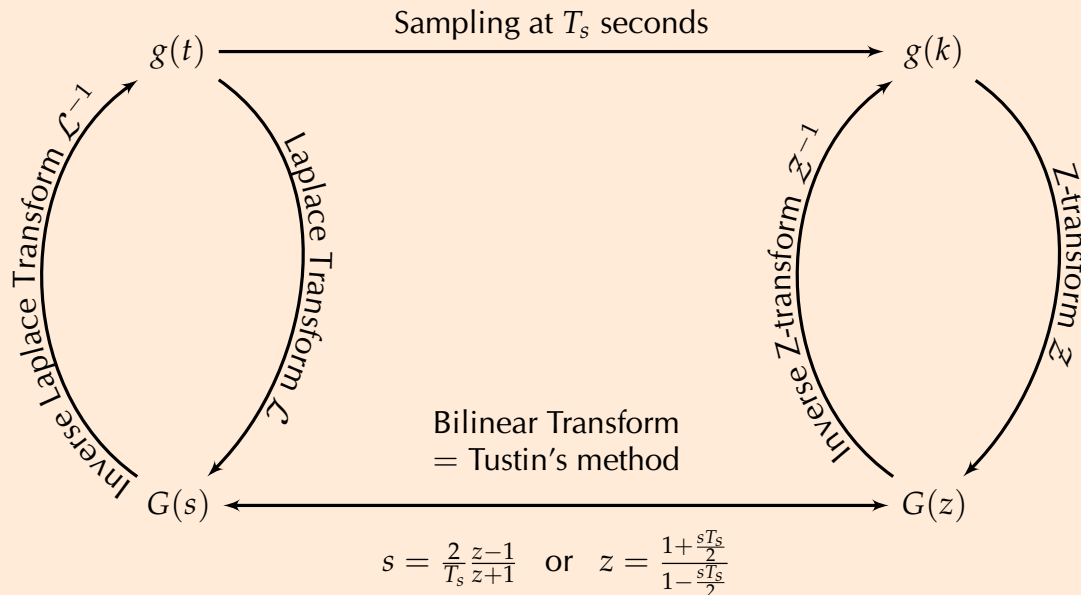


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# Bilinear transform and Z-transform



- Both  $s$ -domain &  $z$ -domain are fictitious domains.
- $s$ -domain simplifies working with differential equations;  $z$ -domain simplifies working with difference equations.
- Bilinear transform is not the only way to go  $G(s) \leftrightarrow G(z)$ .
- $T_s$  determined by Nyquist sampling rate.

$$G(s) \longleftrightarrow G(z)$$

- Consider definitions of  $\mathcal{L}$  and  $\mathcal{Z}$

$$Y(s) = \mathcal{L}\{y(t)\} \triangleq \int_{t=0}^{\infty} y(t)e^{-st}dt$$

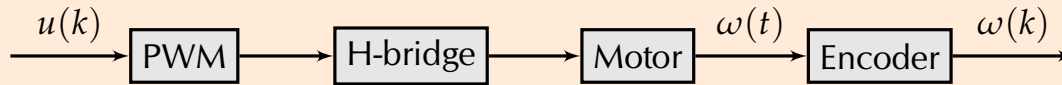
$$Y(z) = \mathcal{Z}\{y(k)\} \triangleq \sum_{k=0}^{\infty} y(k)z^{-k}$$

- Comparison suggests  $z = e^{sT_s}$ .
- To convert  $G(s)$  to  $G(z)$ , can substitute  $s = \frac{\ln z}{T_s}$ .
- Easier to work with an approximation

$$z = e^{sT_s} = e^{\frac{sT_s}{2}} e^{\frac{sT_s}{2}} = \frac{e^{\frac{sT_s}{2}}}{e^{-\frac{sT_s}{2}}} = \frac{1 + \frac{(\frac{sT_s}{2})}{1!} + \frac{(\frac{sT_s}{2})^2}{2!} + \dots}{1 + \frac{(-\frac{sT_s}{2})}{1!} + \frac{(-\frac{sT_s}{2})^2}{2!} + \dots} \approx \frac{1 + \frac{sT_s}{2}}{1 - \frac{sT_s}{2}}$$


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# How Z-transform used in our sys-id



- $u(k)$  denotes sample of  $u(t)$  at sampling instant  $t = kT_s$ .
- Let  $u(k) \rightarrow \omega(k)$  TF be  $G(z)$ .
- Use  $u(k), \omega(k)$  pairs to build  $G(z)$ .
- Use bilinear transform to go from  $G(z)$  to  $G(s)$ .

Important property of Z-transform used:

$$z^{-l}X(z) \leftrightarrow x(k-l) \quad \text{given} \quad X(z) \leftrightarrow x(k).$$



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## What is least squares sys-id? (1/2)

- Let  $G(z) = \frac{b_1z^2 + b_2z + b_3}{z^3 + a_1z^2 + a_2z + a_3} = \frac{Y(z)}{U(z)}$ .

- Cross multiply:

$$b_1z^2U(z) + b_2zU(z) + b_3U(z) = z^3Y(z) + a_1z^2Y(z) + a_2zY(z) + a_3Y(z).$$

- Multiply throughout by  $z^{-3}$ :

$$b_1z^{-1}U(z) + b_2z^{-2}U(z) + b_3z^{-3}U(z) = Y(z) + a_1z^{-1}Y(z) + a_2z^{-2}Y(z) + a_3z^{-3}Y(z).$$

- Take  $\mathcal{Z}^{-1}$  to obtain difference equation

$$b_1u(k-1) + b_2u(k-2) + b_3u(k-3) = y(k) + a_1y(k-1) + a_2y(k-2) + a_3y(k-3).$$


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## What is least squares sys-id? (2/2)

Consider  $b_1u(k-1) + b_2u(k-2) + b_3u(k-3) =$   
 $y(k) + a_1y(k-1) + a_2y(k-2) + a_3y(k-3). \quad (1)$

- Let  $\sigma = [b_1 \quad b_2 \quad b_3 \quad -a_1 \quad -a_2 \quad -a_3]^\top$ .
- Suppose we have data of  $u(k)$  and  $y(k)$  for  $k = 0, 1, \dots, N$ .
- Problem: Find  $\sigma$  such that (1) holds for this data.

I.E., find parameters of a TF that fits to input-output data.

- Let error in the fit be

$$\varepsilon(k, \sigma) = b_1u(k-1) + b_2u(k-2) + b_3u(k-3) - y(k) \\ - a_1y(k-1) - a_2y(k-2) - a_3y(k-3).$$

- Modified problem: Find  $\sigma$  to minimize  $\mathcal{J}(\sigma) \triangleq \sum_{k=0}^N \varepsilon^2(k, \sigma)$ .
- If  $\mathcal{J}(\sigma = \sigma_0) = 0$ , then find best estimate  $\hat{\sigma}$  of  $\sigma_0$ .



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## Part III

# Review of Exp.2: What the experiment taught

- Sys-id techniques from Exp.1 & Exp.2 give different results.
- Likely cause is not only the dead zone nonlinearity in the plant, but also the input signals the sys-id technique uses.  
E.g., the step input ( $u = 7$ ) in Exp.1 does not keep plant in dead zone, while the low-frequency (5 – 10 Hz) triangular input makes the plant go into dead zone twice every cycle.
- Will using rectangular waveform instead of triangular waveform (TW) give a different model with least squares sys-id (LSS)?
- If plant behaves as 1st order even with TW, LSS will say that



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plant has one LHP pole that is 10 – 20 times deeper than the other.



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